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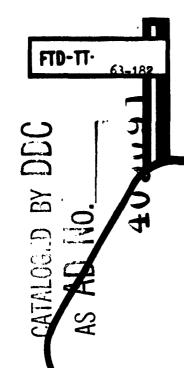
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TRANSLATION

ON THE CONSTANCY OF TANGENTIAL RUPTURE IN A RAREFIED PLASMA

BY

L. D. Pichakhchi

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FOREIGN TECHNOLOGY DIVISION



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BY: L. D. Pichakhchi

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ON THE CONSTANCY OF TANGENTIAL RUPTURE IN A RAREFIED PLASMA

By L. D. Pichakhchi

On the basis of magnetohydrodynamic equations of Chu, Gol'dberg and Lou have been analyzed problesm concerning the constancy of tangential rupture in a plasma. In general, the case of arbitrary parameters, which characterize the rupture obtained an adequate constancy condition, and for a special case, when the jump is experienced only by the speed of the plasma, a zone of constancy was attained.

We like to point out that the plasma is described by a system of magnetohydrodynamic equations by Chu, Gol'dberg and Lou (1-3):

where

$$\rho \frac{\partial v_i}{\partial t} + \rho v_k \frac{\partial v_i}{\partial x_k} = -\frac{\partial \rho_{ik}}{\partial x_k} - \frac{1}{4\pi} H_k \frac{\partial H_k}{\partial x_i} + \frac{1}{4\pi} H_k \frac{\partial H_i}{\partial x_k}. \tag{1}$$

$$p_{ik} = p_1 v_{ik} + \frac{p_1 - p_2}{H^2} H_i H_k, \qquad (2)$$

$$\frac{\partial p}{\partial t} + \operatorname{div} p v = 0, \qquad (3)$$

$$\frac{\partial \rho}{\partial t} + \operatorname{div} \rho v = 0, \tag{3}$$

$$\frac{\partial H}{\partial t} = \text{rot}[vH], \quad \text{div } H = 0, \quad E = -\frac{1}{c}[vH], \tag{4}$$

•
$$\frac{d}{dt} \left(\frac{p_1}{\rho H} \right) = 0, \quad \frac{d}{dt} \left(\frac{p_1 H^3}{\rho^2} \right) = 0.$$
 (5)

Within the frames of the system of equations (1) - (5) the density tensor of the pulse flow and the density vector of the energy flow have the appearance of:

$$\Pi_{ik} = \rho v_i v_k + \rho_{ik} - \frac{1}{4\pi} \left(H_i H_k - \frac{1}{2} \delta_{ik} H^2 \right), \tag{6}$$

$$Q = \rho v \left(\frac{v^2}{2} + \epsilon + \frac{\rho_1}{\rho} \right) + \frac{\rho_1 - \rho_1}{H^2} H(vH) + \frac{1}{4\pi} [H(vH)], \qquad (7)$$

(p + 1 P u) - sought for internal energy of the plasma. Having expressions (6) and (7), the known method (4,5) we obtain easily the conditions for tangential rupture:

$$v_x = 0$$
, $H_x = 0$, $\left\{ \rho_{\perp} + \frac{H^2}{8\pi} \right\} = 0$.

The magnetic field H and speed v lie in the rupture area and experience arbitrary jumps. Density jumps q and pressure anisotropy $a = p_{ij} - p_{ij}$ are also arbitrary, and the pressure p_{ij} is connected with the magnetic field by the relationship (9).

The investigation of constancy of tangential rupture will be conducted by a method, which was utilized in [4] in case of magnetic hydrodynamics with scalar pressure.

At small disturbances of the stationary tangential rupture in the case of arbitrary Heven and also as in[4] it is possible to obtain such conditions for excitations on the surface of separation:

$$\begin{aligned} \Phi_x' &- \frac{\partial \xi}{\partial t} - v_y \frac{\partial \xi}{\partial y} - v_z \frac{\partial \xi}{\partial z} = 0, \\ h_x &- H_y \frac{\partial \xi}{\partial y} - H_z \frac{\partial \xi}{\partial z} = 0, \\ \left\{ p' + \frac{1}{4\pi} (H_y h_y + H_z h_z) \right\} = 0, \end{aligned}$$

where v⁰, h⁰, p⁰ - small excitations of values v₀H,p = p₁, whereby a system of xyz coordinates was derived, bound with the surface of the stationary separation with axis x directed along the normal to the surface; xi - small displacement value of the surface of separation along axis x; the figurative little bows here and further on designate the difference of the closed in them value on both sides of the separation surface.

We linearize the system of equations (1) - (5). To solve
$$\exp i(kr - \omega t) \tag{//}$$

we obtain such a system of linear equations: $\omega_0 \mathbf{v}' - \frac{1}{\rho} \left(\rho' + \rho \mathbf{u} \mathbf{u}' \right) \mathbf{k} + \left(\mathbf{k}_0 \mathbf{u} \right) \left(1 - \frac{a}{\rho \mathbf{u}^2} \right) \mathbf{u}' - \frac{a}{\rho \mathbf{u}^2} (\mathbf{k}_0 \mathbf{u}) \left(\frac{a'}{a} - 2 \frac{\mathbf{u} \mathbf{u}'}{\mathbf{u}^2} \right) \mathbf{u} = 0,$

$$(kv') = \omega_0 \frac{p'}{p}, \qquad (13)$$

$$(ku') = 0, (14)$$

$$\omega_0 u' + (k_0 u) v' - (k v') u = 0,$$
 (15)

$$\omega_{\phi}\left(\frac{p'}{p}-\frac{p'}{p}-\frac{\mathbf{u}\cdot\mathbf{u}'}{u^2}\right)=0, \qquad (/6)$$

$$\omega_0\left(\frac{a'+p'}{a+p}+2\frac{\mathbf{u}\cdot\mathbf{u}'}{\mathbf{u}^2}-3\frac{p'}{p}\right)=0. \tag{7}$$

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Here are introduced designations $w_0 = \omega - (k_0 v)$, $u = \frac{H}{V4R}$, u^1 , a^1 -small excitations of values u, a; $k_0(0,k_v,k_z)$ -true instantaneous vector at the plane of separation. In writing equations (12)-(17) are included conditions (8).

Eliminating solutions $\omega_e = 0$, which offer true values and can therefore not lead to inconstancy, and eliminating v', we will obtain:

$$\left[(k_{\theta}u) \left(1 - \frac{a}{\rho u^{2}} \right) - \frac{\omega_{0}^{2}}{(k_{\theta}u)} \right] u' - \frac{1}{\rho} (\rho' + \rho u u') k -$$

$$- \left[\frac{a}{\rho u^{2}} (k_{0}u) \left(\frac{a'}{a} - 2 \frac{u u'}{u^{2}} \right) - \frac{\omega_{0}^{2}}{(k_{\theta}u)} \frac{\rho'}{\rho} \right] u = 0, \qquad (18)$$

$$(ku') = 0, \qquad (29)$$

$$\frac{\rho'}{\rho} - \frac{\rho'}{\rho} - \frac{u u'}{u^{2}} = 0, \qquad (20)$$

$$\frac{a'}{a} + \frac{\rho'}{a} + 2 \left(1 + \frac{\rho}{a} \right) \frac{u u'}{u^{2}} - 3 \left(1 + \frac{\rho}{a} \right) \frac{\rho'}{\rho} = 0. \qquad (21)$$

Formulating equations (18) by k and u, with consideration of (19) we will obtain together with equations (20) and (21) a system of four uniform equations for the unknown **; *; *. The characteristic determinant of this system is equalized to zero and we obtain equations which bind w and ka

$$\omega_0^4 - \omega_0^2 \left[k^2 u^2 (1 + 2P) + (k_0 u)^2 (2A + P) \right] + \\ + (k_0 u)^2 \left[k^2 u^2 (3A + 3P + 6AP + 5P^2) - (k_0 u)^2 (3A^2 + 9AP + 5P^2) \right] = 8$$

$$A = \frac{a}{2u^2}, \quad P = \frac{p}{2u^3}. \tag{22a}$$

where

If in this equation is written that $k = k_0$, it will designate phase expansion rates of small excitations with instantaneous vectors, which lie in the plane of separation:

(23) $V_{1,2} = v_0 \pm V_{21}$ $V_{3,4} = v_0 + V_{41}$

where

$$V_s = \sqrt{\frac{D}{2} - \sqrt{\frac{D^2}{4} - F}}, \quad V_f = \sqrt{\frac{D}{2} + \sqrt{\frac{D^2}{4} - F}}, \quad (234)$$

$$a D = u^2 [1 + 2P + \mu^2 (2A + P)],$$

$$F = u^4 \mu^2 [3A + 3P + 6AP + 5P^2 + \mu^2 (3A^2 + 9AP + 5P^2)].$$

It should be rointed out, that the velocities Vs and Vf - actually values, for which it is necessary that

$$F > 0$$
: $\frac{D^2}{4} - F > 0$. (24)

Complex values V_8 or V_1 would indicate, that the plasma is unstable with respect to small excitations [2,6], irrespective of the tangential separation (rupture). From such considerations we will assume as fulfilled the conditions at which to the actual values k in equation (22) correspond actual values ω . From it under such conditions should arise the condition of positiveness of the free member in (22). Including (24) this gives: $3A \pm 3P \pm 6AP \pm 5P^2 > 0. \tag{2.57}$

Instability can be caused only by complex values k_x (we assume that k_0 -actual value). We will take x - component of equation (18) and utilizing boundary conditions (10) which for solving (11), after inclusion of xi give:

$$\{p' + \rho u u'\} = 0; \quad \{u'_x \mid (k_0 u)\} = 0,$$

we will obtains

$$\left| \frac{P}{h_x} [(N_0 u)^2 (1 - A) - \omega_0^2] \right| = 0. \tag{26}$$

From equation (22) we find k, and substitute in (26)

$$\frac{\sqrt{1-\frac{(V-v_1v_1)^4-(V-v_1v_1)^2\mu_1^2u_1^2(2A_1+P_1)-\mu_1^4u_1^4(3A_1^2+9A_1P_1+5P_1^6)}{u_1^2((V-v_1v_1)^2(1+2P_1)-\mu_1^2u_1^2(3A_1+3P_1+6A_1P_1+5P_1^2)}}{\rho_1\left[\mu_1^2u_1^2(1-A_1)-(V-v_1v_1)^2\right]}=$$

$$-\frac{\sqrt{1-\frac{(V-v_2v_3)^2-(V-v_2v_3)^2}{u_1^2[(V-v_2v_3)^2(1+2P_3)-\mu_1^2u_2^2(3A_g+3P_2+5P_3^2)}}{\frac{u_1^2[(V-v_2v_3)^2(1+2P_3)-\mu_1^2u_2^2(3A_g+3P_2+6A_2P_3+5P_3^2)}{\rho_2[\mu_1^2u_2^2(1-A_3)-(V-v_2v_3)^2]}}$$

where $V = k_0$. The signs k_{x1} and k_{x2} were selected so that the excitations remained finite at an increase in/x/, whereby it is also necessary to place a requirement, that the true parts of the radicals should be positive. At any values of parameters, equation (27) for V may have complex roots with positive imaginary part, which will indicate inconstancy of separation (rupture). Equation (27) can be written, by introducing speeds V_n and V_n as well as

$$V_A = \mu u \sqrt{1-A}, \quad V_m = \mu u \sqrt{\frac{3A+3P+6AP+5P^2}{1+2P}}$$
 (26)

(we like to point out that with respect to formulas (24) and (25) V_A and V_m - actual values) in form of $\sqrt{(V-v_1v_1-V_2)(V-v_1v_1+V_2)(V-v_1v_1+V_2)}$

$$\frac{\sqrt{\frac{(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s1})(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s1})}{(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s2})}}{\frac{(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s2})}{(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s2})}}{\frac{(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s2})(V-v_1v_1+V_{s2})}{(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s2})}}$$
= -d \[
\frac{(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s2})(V-v_1v_1+V_{s2})}{(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s2})} \]
(29)

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We will present (29) in a square and bring it into form of

$$(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s1})(V-v_1v_1-V_{s1})(V-v_1v_1+V_{s1})\times \\ \times (V-v_2v_2-V_{ss2})(V-v_2v_2+V_{ss2})(V-v_2v_2-V_{ss2})(V-v_2v_2+V_{ss2})^2 = \\ = d^2(V-v_1v_2-V_{ss2})(V-v_2v_2+V_{ss2})(V-v_2v_2-V_{ss2})(V-v_2v_2+V_{ss2})\times \\ \times (V-v_1v_1-V_{ss1})(V-v_1v_1+V_{ss1})(V-v_1v_1-V_{ss2})^2 (V-v_1v_2+V_{ss2})^2.$$
(30)

Now is possible to express such adequate condition of tangentic1 separation constancy.

We will arrange all speeds $\gamma_1 v_1 + v_{s1}$, $\gamma_1 v_1 - v_{s2}$... $\gamma_2 v_2 - v_{s2}$, $\gamma_2 v_2 + v_{s2}$... $\gamma_i v_1 - v_{s2}$ Valo which are included in (30) in the order of their increase. Since the speeds. included in the left half of the equation, alternate with the velocities, included in the right half, and in addition they alternate and are "multiple" of velocities 32v2 + VA2. 7172 - VA2 of the left half with the "multiple" velocities Q1V, + VA1. 72V1 - VA1 of the right half of the equation, then all roots of equation (30), and also equation (27), will be actual and the tangential separation (rupture) will be constant.

Next we will investigate equation (27) for the case when we tors vieve units are par 1ell. when ¬1 = ¬2 = µ1 = µ2 ≥ ¬•

For small values v, imaginary roots V, if they do exist, tend toward zero with , consequently the second member under the radical equalling unity can be disregarded. We obtain equations

$$g_1[v^2u_1^2(1-A_1)-(1-vv_1)^2]=-g_2[v^2u_2^2(1-A_2)-(1-vv_2)^2], \qquad (3)$$

from which it is evident, that separation (rupture) will be constant upon fulfillment of condition

$$\rho_1 u_1^2 (1 - A_1) + \rho_2 u_2^2 (1 - A_2) - \frac{\rho_1 \rho_2}{\rho_1 + \rho_2} (\nu_2 - \nu_1)^2 > 0.$$
 (32)

In case of arbitrary , we will limit the class of separations by an additional requirement

$$a_1 = b_2 \equiv y$$
, $a_1 = a_2 \equiv a$, $u_1 = u_2 \equiv u$, $p_1 = p_2 \equiv p$ (33)

and will introduce a system of coordinates, in which

$$v_1 = -\frac{v_2 - v_1}{2} = -\frac{v_0}{2}, \quad v_2 = \frac{v_2 - v_1}{2} = \frac{v_0}{2}.$$
 (55d)

In this case it will be convenient to utilize equation (29), in which should be

$$d=1, \quad V_{s1}=V_{s2}\equiv V_{s}, \quad V_{f1}=V_{f2}\equiv V_{f}, \quad V_{m1}=V_{m2}\equiv V_{m}, \quad (34)$$

$$V_{A1}=V_{A2}\equiv V_{A}, \quad v_{1}=-\frac{v_{0}}{2}, \quad v_{2}=\frac{v_{0}}{2}.$$

When $\gamma = 0$ for separations (33) conditions (32) transform into condition

$$V_{\lambda} > \frac{v_a}{2}. \tag{3.5}$$

In the other boundary case 49 = 1 equation (29) (in which conditions (34) are included after after increasing into square, provided we eliminate the true roots $\omega = 0$ and $\omega = \pm (\frac{v_0}{2} \pm v_1)$, transforms into

$$V^{4} - 2\left(V_{s}^{2} + \frac{v_{0}^{2}}{4}\right) V^{2} + \left(\frac{v_{0}^{2}}{4}\right)^{2} - 2\left(\frac{v_{0}^{2}}{4}\right) V_{s}^{2} + \\ + V_{A}^{2}\left(V_{s}^{2} - V_{m}^{2}\right) + V_{s}^{2}V_{m}^{2} = 0,$$
(34)

where

$$V_s = u\sqrt{3(A+P)}, \quad V_m = u\sqrt{3(A+P) - \frac{P^2}{(1+2P)}}, \quad V_A = u\sqrt{1-A}$$
 (36 a)

We will divide (36) into
$$V_s^{\mu}$$
 and introduce designations:
$$\frac{V_A^2}{V_s^2} = \alpha^2, \quad \frac{V_B^2}{V_s^2} = 1 - \frac{P^2}{(1+2P)(3A+3P)}, \quad \frac{v_0^2}{4V_s^2} = \beta^2, \quad \frac{V^2}{V_s^2} = x^2, \quad \text{nphrony } \alpha, \beta, \gamma > 0.$$

we will obtain

$$z^{4}-2x^{2}(1+\beta^{2})+\beta^{4}-2\beta^{2}+\gamma\alpha^{2}+1-\gamma=0.$$
 (37)

Equation (37) has purely imaginary roots, because

$$(1-\beta^2)^2-\gamma(1-\alpha^2)<0, (38)$$

and complex roots, because

$$49^2 + y(1-a^2) < 0.$$
 (37)

To the inequalities (38) and (39) should be added inequality

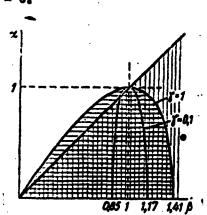
$$1-\gamma>0, \tag{40}$$

which is the result of inequality (25).

A direct check will convince, that the values alpha and beta , which satisfy in equality (39), should be eliminated by the fact, that the positiveness condition

of actual parts of radicals in (27) is not fulfilled here. In this way the inconstancy may originate only for alpha and beta values which do satisfy the inequality (38).

On the drawing are shown zones of inconstant separation (hatched by horizontal lines) for two values on masO.1; l. For carma 0 this zone is contracted into the section of straight beta = 1. On the drawing is drawn a straight line alpha = beta which separates the constancy zone from the inconstancy zone (hatched by vertical lines) of separation for V = 0.



We shall now discuss intermediate values 0 < 0 < 1. Excitations, corresponding to these

values > can be considered as a superposition

of two excitations, which correspond to values v = 0 and v = 1. Considering the fact that

equation (10), (12) - (17) are linear, solutions for each one of the excitations will

be independent and in agreement with the

shready obtained for v = 0 and v = 1. Furthermore, figuring, that not the value of excitation amplitude, nor absolute values k_0 affect the found zones of instability then for any arbitrary $0 \le v \le 1$ both zones exist together. For example, when gamma =1 the instability zone will be the entire hatched part of the area alpha and beta (see drawing).

In conclusion I want to express sincere thanks to prof.V.L.German for the work proposed by him.

Literature

- 1.G.F.Chew, M.L.Goldberger, F.S.Low, Proc.Roy.Soc.A.236,112,1956 (its translation at PSF No.7,139, 1957).
 - 2. R.Y. Polovin, H.L. Tsintsadze, Ukrainskiy Fizicheskiy Zhurnal 4,30,1)59
- 3. I.A.Alchiezer, R.V.Folovin, H.L.Tsintsadze, Zhurnal Eksperimontal'noy i Teoreticheskoy Fiziki, 37,756, 1959.
 - 4. S.I.Syrovatskiy.Transactions of Phys.Inst.8,15,1956
 - 5. L.D.Landau, Ye.M.Lifchits, Electrodynamics of Solid Media, CITTL, Moscow, 1957
- 6. R.Z.Sardayev. collection of rep. Physics of Plasma and Problems of Controlled Thermonuclear Reactions vol. 7. Izdat. Akad. Hauk. SSSR, Moscow 1958. p. 268

7.A.G. Murosh, Course in Higher Algebra COIZ, Gostekhizdat, 1946.

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